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AYOQCHI GRUNTLI TO'G'ONINING DINAMIK HOLATINI REZONANS REJIMI ATROFIDA TEKSHIRISH

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Annotatsiya: *Inshootlarning xususiy tebranish chastotalari va shakllari, inshootning asosiy parametrlarini tashkil qiladi va inshootning dinamik xususiyatlari deb ataladi. Dinamik xususiyatlar inshoot bo'yicha katta ma'lumotlarni jamlagan bo'lib, u inshootning pasporti hisoblanadi.*

Bir jinssiz bo'lgan gruntli to'g'onlarning xususiy tebranish chastotalarini aniqlash masalasi murakkab masala hisoblanadi. Shuning uchun ko'p hollarda hech bo'lmasa birinchi yaqinlashuvda, asosiy hisobiy parametrlarga ega bo'lish maqsadida, inshootlarning o'ta taqribiy hisoblash sxemalaridan foydalanishga to'g'ri keladi.

Kalit so'zlar: *Gidrotexnika, gruntli inshootlar, seysmika, tebranishlar.*

Ushbu bo'limda Ayoqchi gruntli to'g'oni real geometriyasini, inshootning xususiy og'irligi va grunt materialining dissipativ xususiyatni hisobga olgan holdagi noturg'un majburiy tebranishlari tahlil qilindi.

Bu holda qaralayotgan masala quyidagi boshlang'ich shartlar bilan birgalikda $u(0)=u_0$, $\dot{u}(0)=\dot{u}_0$ bo'lgan holda ikkinchi tartibli ko'p sonli oddiy differensial tenglamalar sistemasini yechishga keltirilada, ya'ni:

$$\begin{aligned} [M]\{\ddot{u}\} + [C]\{\dot{u}(t)\} + [K]\{u(t)\} &= \{P(t)\} \\ u(0)=u_0, \dot{u}(0)=\dot{u}_0 \end{aligned} \quad (1)$$

Bu tenglamalarda quyidagi belgilashlar qabul qilingan:

$[K]$, $[M]$ – to'g'onning bikirlik va massa matritsalar; $[C]$ - tugun materialining dissipativ xususiyatini ifodalovchi dempferlik matritsa; $\{u\}$ - tashqi kuch (kinematik ta'sir) natijasida to'g'on tugunlaridagi inshootning izlanayotgan tugun ko'chishlarining vektor komponentalari; $P(t)$ - kinematik ta'sir natijasida to'g'on tugunlariga ta'sir qiluvchi dinamik kuch.

(1) – differensial tenglamalar sistemasi Nyumark usuli yordamida yechildi.

Masalani yechishda to'g'on asosiga ta'sir qiluvchi gorizontol kinematik ta'sir quyidagi ko'rinishda olindi:

$$\ddot{U}^0 = A * \sin(2\pi * p * t) \quad (2)$$

bu yerda $A=a*p^2$ – ta'sir kilayotgan kinematik tezlanishning amplitudasi;



ρ - kinematik ta'sirning chastotasi.

Hisob ishlarini bajarishda kinematik ta'sirning qiymatlari quyidagicha olindi:

$A=0.3 \text{ m/cek}^2$ - bu taxminan 8 ballik yer qimirlash jarayoniga to'g'ri keladi; $t=20 \text{ cek}$; $\rho \approx \omega_1=1.0449 \text{ Gs}$ -kinematik ta'sirning chastotasi. Material uchun dempferlik matritsa $[C]$ quyidagi ko'rinishda qabul qilindi:

$$[C]=2\varepsilon[M] \quad (3)$$

bu yerda ε – o'zgarmas son (materialning dempferlash koeffitsiyen ti) bo'lib, uning qiymati gruntdagi energiyaning yutilish koeffitsiyenti ψ orqali ($0,2 \leq \psi \leq 0,35$), $\omega_1 \approx 1 \text{ Gs}$ atrofida bo'lganida quyidagi formulasi orqali aniqlandi.

$$\psi = \frac{4\pi\varepsilon}{\omega_1}, \quad (4)$$

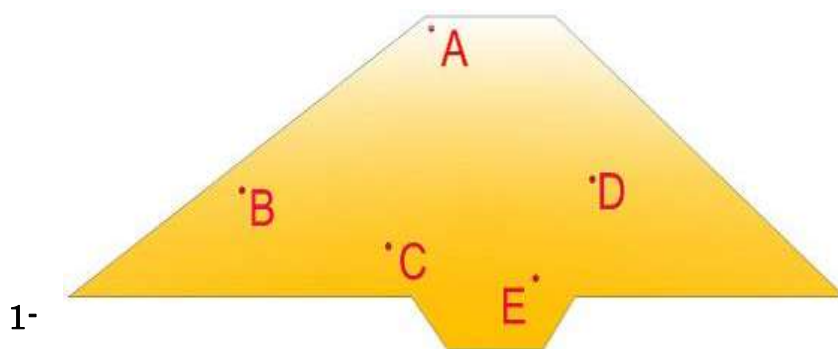
ya'ni:

$$0,06 \leq \varepsilon \leq 0,12 \text{ bo'lgani uchun}$$

(ε) ning qiymati gruntli to'g'onning dinamik holatini baholashda, $\varepsilon=0.1$, deb olindi.

Hisob ishlarini bajarishda 1 – rasmda ko'rsatilgan to'g'on tanasida belgilab olingan A,B,C,D va E nuqtalardagi xususiy og'irlik va kinematik ta'sir (2) natijasida t vaqt oralig'ida noturg'un majburiy tebranishlarning natijalari 2 va 3-rasmlarda keltirilgan.

2 va 3 rasmlarda to'g'on tanasidagi turli nuqtalarning (1-pacm) ko'chishlarini vaqt bo'yicha o'zgarish ko'rsatkichlari kinematic ta'sirning chastotasiga taxminan teng bo'lgan ($\rho \approx \omega_1=1.0449 \text{ Gs}$) holat uchun olingan.



1-

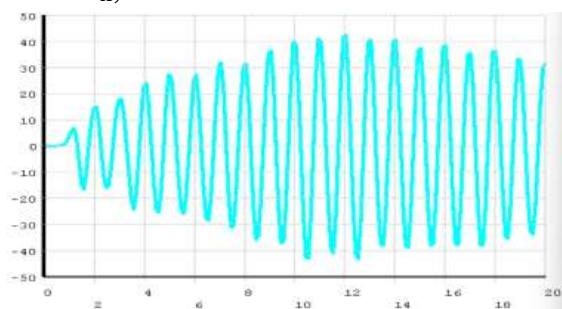
rasm. Ko'chish
komponentalari

aniqlangan to'g'onning turli nuqtalari



A: $x=182.5; y=65$ (m)

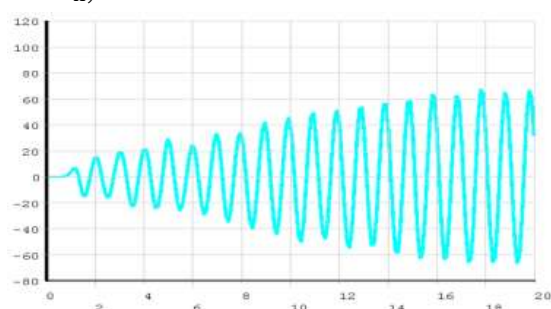
U_x, m



t, sek

A: $x=182.5; y=65$ (m)

U_x, m

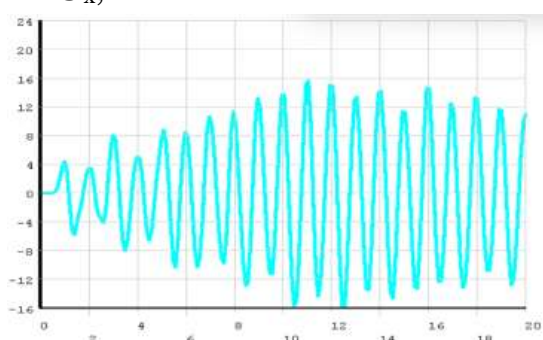


t,

sek

B: $x=40.98; y=50$ (m)

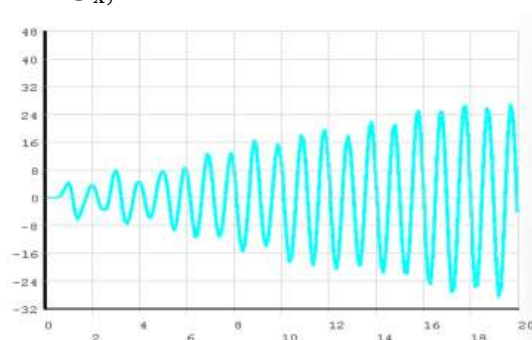
U_x, m



t, sek

B: $x=40.98; y=50$ (m)

U_x, m

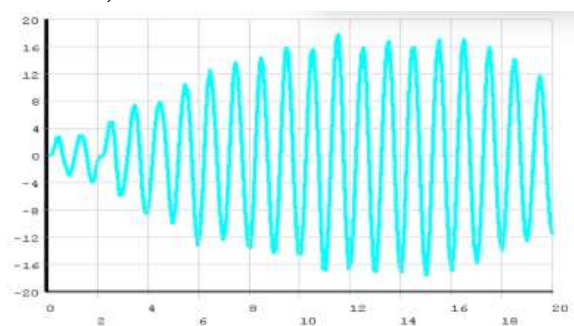


t,

sek

C: $x=168.46; y=18$ (m)

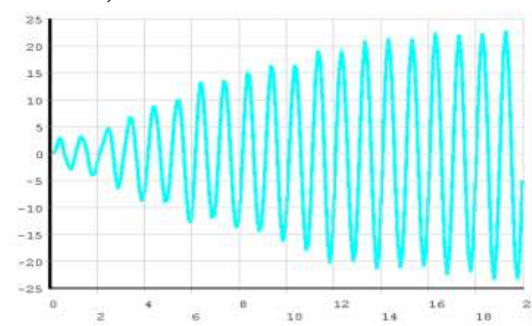
U_x, m



t, sek

C: $x=168.46; y=18$ (m)

U_x, m



t,

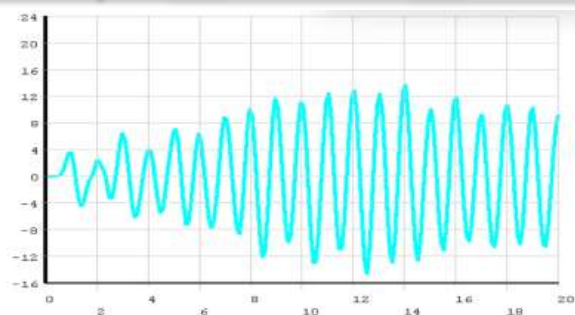
sek

D: $x=259.38; y=45$ (m)

U_x, m

D: $x=259.38; y=45$ (m)

U_x, m

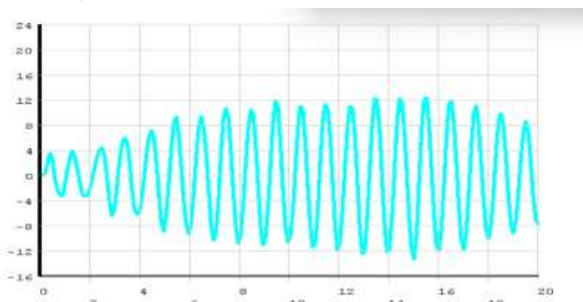


t,

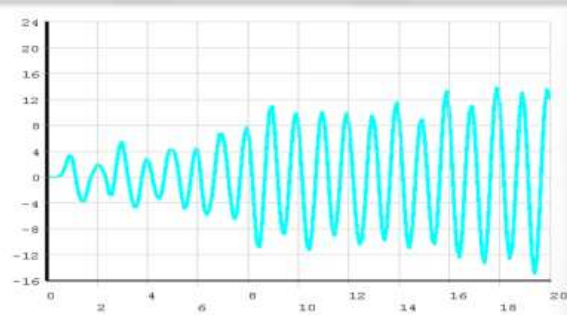
sek

E: $x=192.17; y=8$ (m)

U_x, m



t, sek

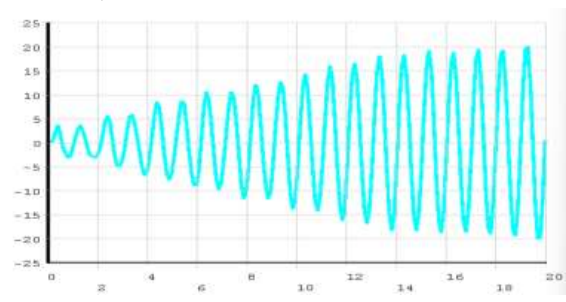


t,

sek

E: $x=192.17; y=8$ (m)

U_x, m



t,

sek

2-rasm. Bir jinsli Ayoqchi gruntli to'g'onining A,B,C,D va E nuqtalaridagi gorizantal kuchishlarning vaqt bo'yicha o'zgarishi

3-rasm. Bir jinsli bo'lmagan Ayoqchi gruntli to'g'onining A,B,C,D va E nuqtalaridagi gorizantal kuchishlarning vaqt bo'yicha o'zgarishi

Olingan natijalardan ko'rinadiki, tashqi ta'sirning chastotasi gruntli to'g'onning birinchi xususiy tebranish chastotasi (ω_1) ga taxminan yaqin bo'lgan kinematik ta'sirning davomiyligi ($t^*=20$ sekund gacha) bo'lganda inshootning barcha nuqtalardagi tebranish amplitudalari monoton ravishda o'sib borib, rezonans holatini vujudga keltiradi. Bir jisli bo'lgan holat uchun alohida ahamiyat qaratadigan bo'lsak, nuqtalardagi tebranish chastotasi (ω) ma'lum (t) vaqt oralig'ida ochib, keyin asta-sekin pasayib borishini ko'rishimiz mumkin. Bu asosan bir jinsli bo'lgan holat uchun kuzatilmoqda, dastlabki $t=0 \div 5$ sekund oralig'ida tebranish amplitudalari kichik qiymatlarga ega bo'lib, sekin-asta o'sib boradi. Bu holat tashqi ta'sir chastotasining to'g'onning birinchi xususiy tebranish chastotasi (ω_1) ga yaqin kelishi natijasida rezonans ta'sirining yuzaga kelishini kuzatishimiz mumkin. Keyingi $t=5 \div 15$ sekund oralig'ida amplituda qiymatlari sezilarli darajada ortib, maksimal qiymatlarga yetadi. Bu davrda grunt tanasi tashqi tebranish energiyasini to'liq qabul qiliadi natijada kuchlanish komponentlarining amplitudalari ham yuqori darajaga yetadi. Olingan ushbu natija, ya'ni tashqi ta'sirning chastotasi, to'g'onning birinchi



xususiy tebranish chastotasida rezonans holati ro'y berishi EHM dasturini ishonchliligini ko'rsatadi.

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